

Name:	
Enrolment No:	

UNIVERSITY OF PETROLEUM AND ENERGY STUDIES

End Semester Examination, May 2021

Program Name : B. Tech. (APE-Gas)

Semester : III

Course Name : Air Fractionation and Purification of Gases

Time : 3 hr

Course Code : CHGS 4002

Max. Marks: 100

Nos. of page(s) : 3

Instructions: Assume any missing data. The notations used here have the usual meanings. Draw the diagrams, wherever necessary.

SECTION - A (6 × 5 = 30 marks)

(Answer all the questions)

		Marks	CO
1.	Discuss the applications of Argon.	5	CO1
2.	Differentiate between the Linde and Claude cycle used for liquefaction	5	CO3
3.	What are the modifications suggested to improve the thermodynamic efficiency in Oxyton development?	5	CO2
4.	Differentiate between the food grade and nonfood grade carbon dioxide.	5	CO1
5.	What are the factors that affect the separation efficiency in case of membrane separation?	5	CO4
6.	Discuss the three factors affecting the optimum recovery of Argon in liquid plants.	5	CO5

SECTION - B (5 × 10 = 50 marks)

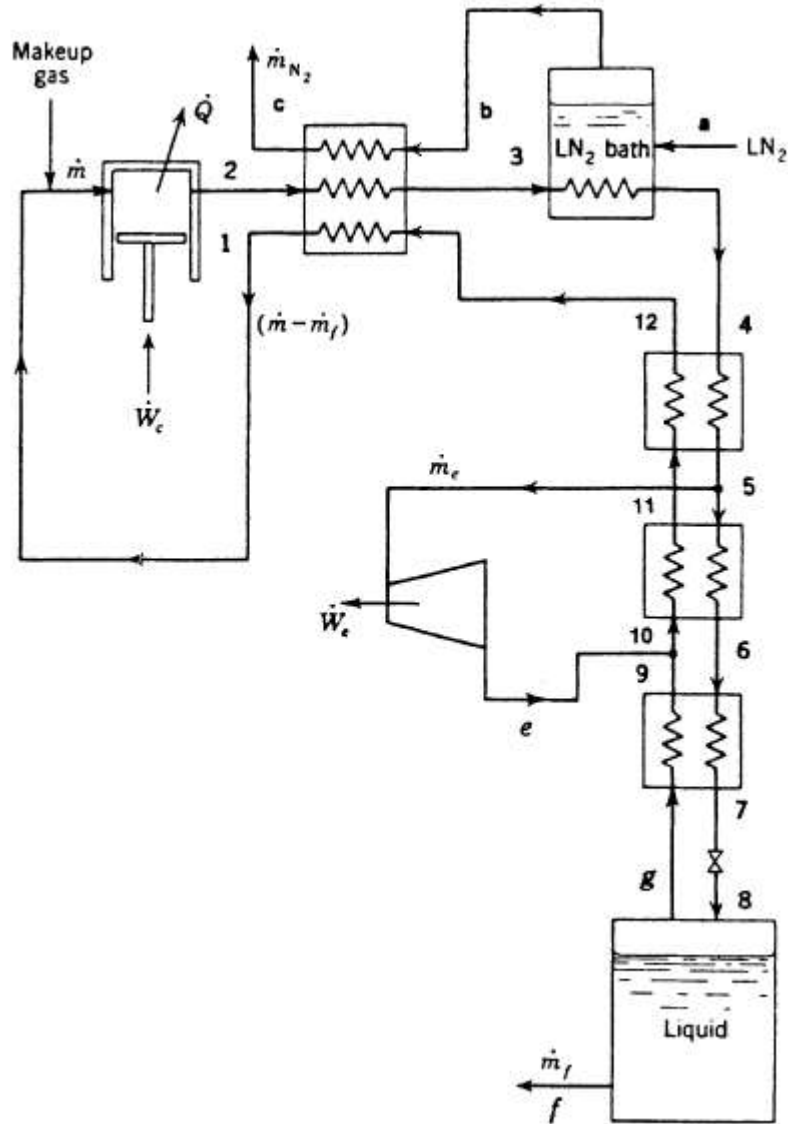
(Answer all the questions)

1.	Discuss the functions of the three operating control valves in the operation of a standard air separation plant.	10	CO5
2.	Define the Lachmann principle. Discuss the thermodynamic analysis of the Oxyton cycle.	10	CO2
3.	Discuss the recovery of carbon monoxide and hydrogen from partial oxidation of methane using a methane wash by absorption followed by fractionation.	10	CO3
4.	Discuss the separation of oxygen using vacuum pressure swing adsorption (VPSA).	10	CO4
5.	Explain the total recovery of helium from the natural gas with the help of a flow diagram.	10	CO2

SECTION – C (1 × 20 = 20 marks)

(Answer all the questions)

1.	A large hydrogen liquefaction plants uses a precooled Claude cycle with one expander similar to that shown in Fig.	20	CO4
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This system could also be used as a refrigerator to cool helium gas. For the operating conditions shown below, determine the following:

- The liquefaction rate of parahydrogen when the system is used as a liquefier;
- The rate of liquid nitrogen consumption for the liquefier;
- The amount of helium gas ($C_p = 2.5 R$) that can be cooled from 25 to 20 K under steady-state conditions when the system is used as a refrigerator (assume that the helium behaves as an ideal gas at this temperature and pressure)
- The rate of liquid nitrogen consumption for the refrigerator in part (c).

Operating Conditions:

Parahydrogen compressed is $\text{XXX} \times 10^{-3} \text{ kg/s}$, where **XXX** is last three digits of SAP ID for both liquefier and refrigerator.

Temperatures of all streams on warm-side of three-channel heat exchanger are 293 K.

Compressor operates between 0.101 and 1.01 MPa.

Inlet temperature to expander is 60.8 K.

70 % of parahydrogen diverted through expander.
Assume ideality for expander, compressor, and heat exchangers.
The liquid nitrogen bath operates at a pressure of 0.101 MPa.

The thermodynamic properties for parahydrogen are as follows:

$$h(0.101 \text{ MPa}, 293 \text{ K}) = 4100 \text{ kJ/kg}$$

$$S(0.101 \text{ MPa}, 293 \text{ K}) = 64.5 \text{ kJ/kg-K}$$

$$h(1.01 \text{ MPa}, 293 \text{ K}) = 4100 \text{ kJ/kg}$$

$$S(1.01 \text{ MPa}, 293 \text{ K}) = 55 \text{ kJ/kg-K}$$

$$h(1.01 \text{ MPa}, 77.3 \text{ K}) = 780 \text{ kJ/kg}$$

$$h(1.01 \text{ MPa}, 60.8 \text{ K}) = 590 \text{ kJ/kg}$$

$$S(1.01 \text{ MPa}, 60.8 \text{ K}) = 32 \text{ kJ/kg-K}$$

$$h(0.101 \text{ MPa}, 77.3 \text{ K}) = 808 \text{ kJ/kg}$$

$$h(0.101 \text{ MPa}, 20.4 \text{ K}) = -256 \text{ kJ/kg}$$

$$S(0.101 \text{ MPa}, 20.4 \text{ K}) = 8 \text{ kJ/kg-K}$$

$$h(0.101 \text{ MPa}, 77.3 \text{ K}) = 29 \text{ kJ/kg}$$

$$h(0.101 \text{ MPa}, 293 \text{ K}) = 455 \text{ kJ/kg}$$

For an ideal expander

$$S_e = 32 \text{ kJ/kg-K} \text{ at } 0.101 \text{ MPa}, h_e = 235 \text{ kJ/kg.}$$